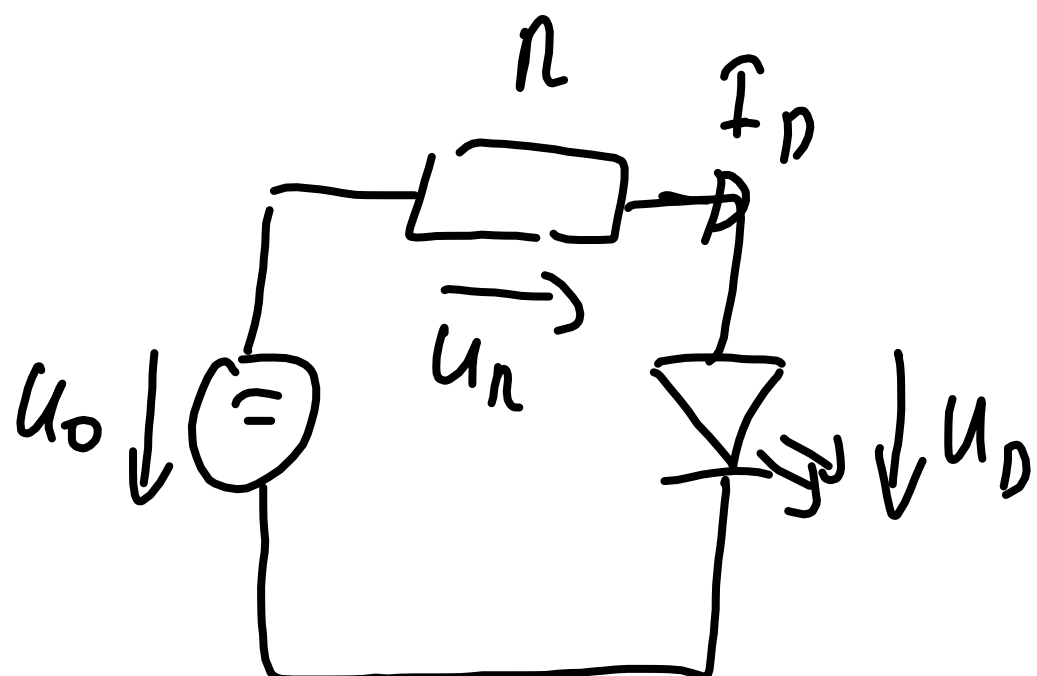


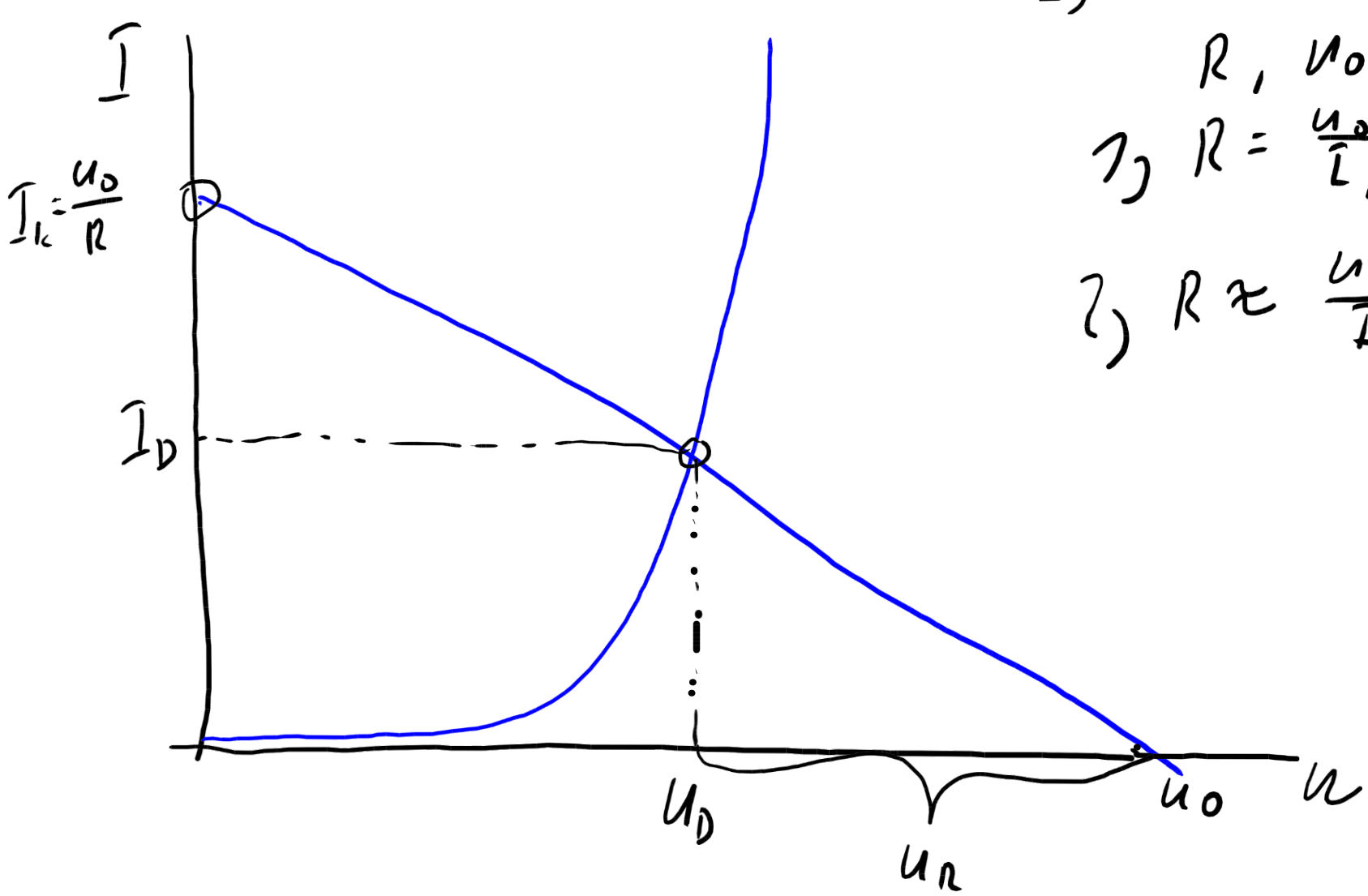
- ΔΙΟΔΗ + ΟΜΠΩΝ

→ ζητάμε I_D, U_D
 + U_0 ΔΙΟΔΙΤΗΣ
 $R = ?$



$R = \frac{U_0}{I_D}$ $\frac{U_R}{I_D}$!

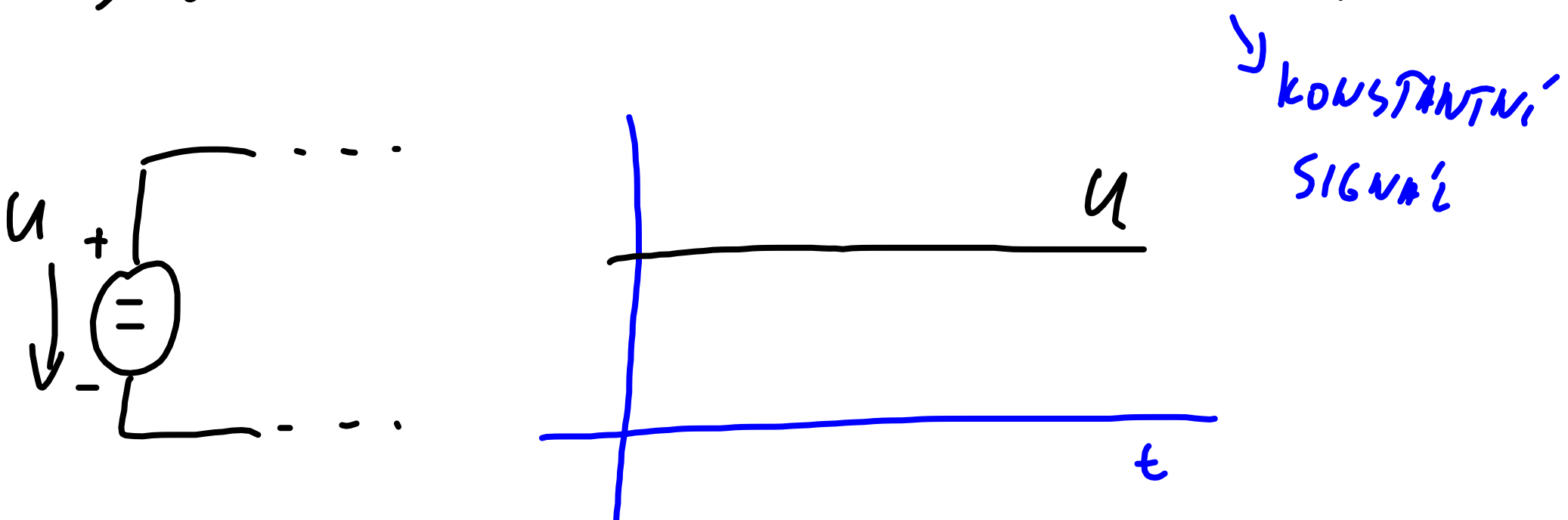
I . ΚΙΝ. ΖΗΤΗΣΗ
 $U_R = U_0 - U_D$



→ ζητάμε I_D
 $R, U_0 = ?$
 1) $R = \frac{U_0}{I_k}$
 2) $R \approx \frac{U_R}{I_D}$

VÝPOČTY V OBVODNĚCH SE STŘÍDMOU (HARMONICKOU) ZDROJEM NAPĚTÍ

- STEJNO SMĚRNÉ ZDROJE NAPĚTÍ (DC)



METODY ŘEŠENÍ: - METODA ZJEDNODUŠOVÁNÍ

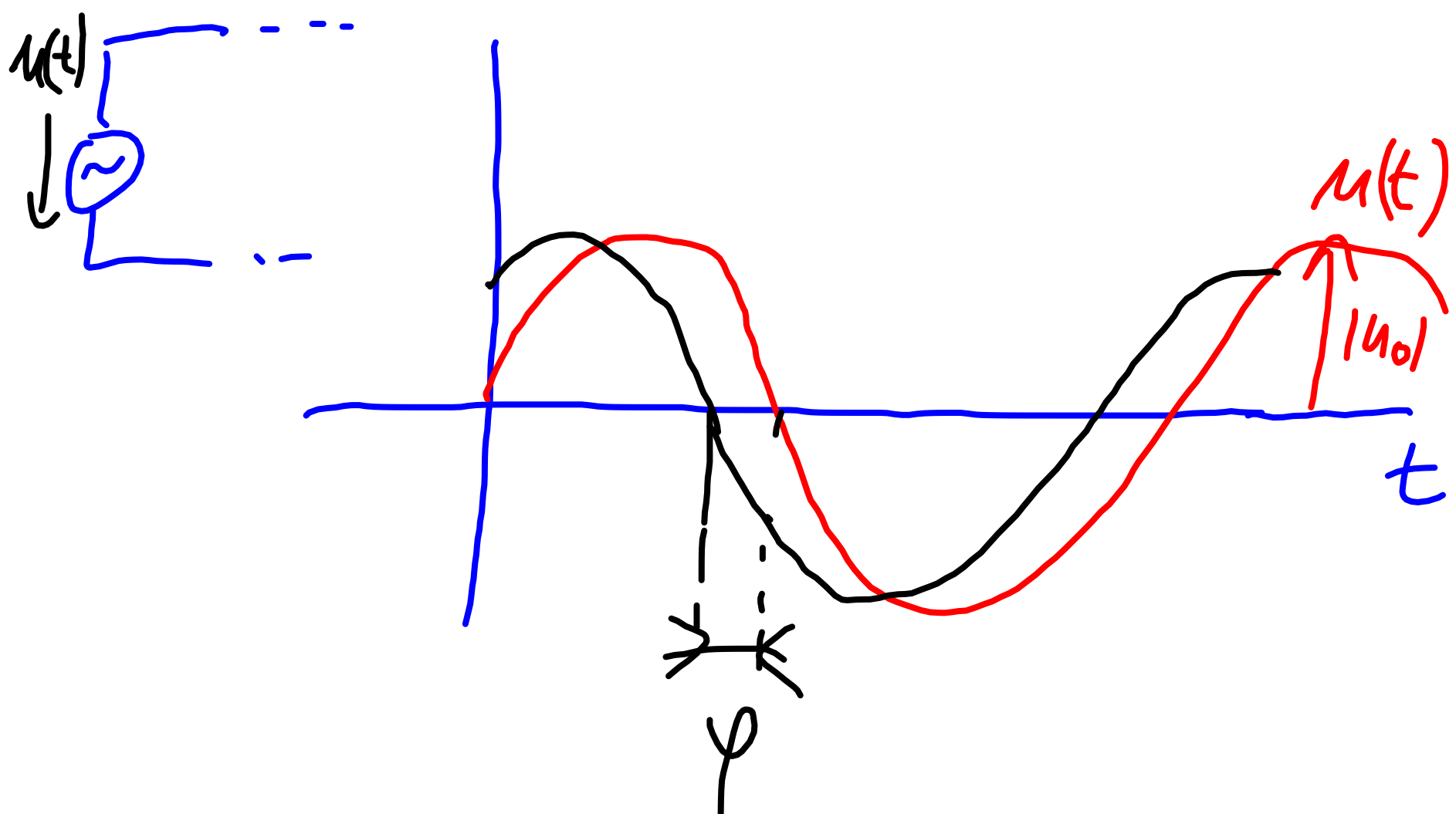
- METODA KĚLOVÝCH NAPĚTÍ

- - II - SYČKOVÝCH PROUDŮ

- THEVENINŮV TEOREM

⋮

- STŘÍDMOU ZDROJEM NAPĚTÍ (AC) → HARMONICKÝ
SIGNÁL



$$u(t) = \underline{U_0} \sin(\omega t + \underline{\varphi})$$

→ ŘEŠÍME USTÁLENÝ STAV

⇓

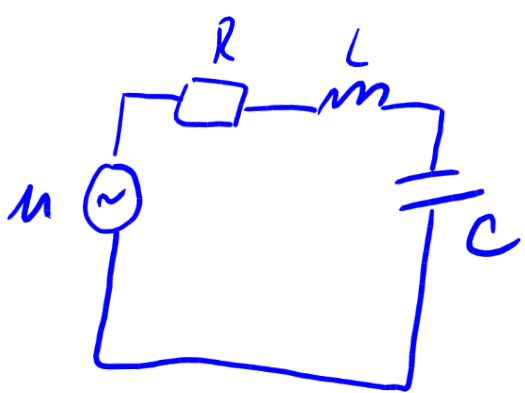
AMPLITUDE + FÁZOVÉ POSUNY

→ STEJNÉ METODY (JAKO U DC OBVODŮ)

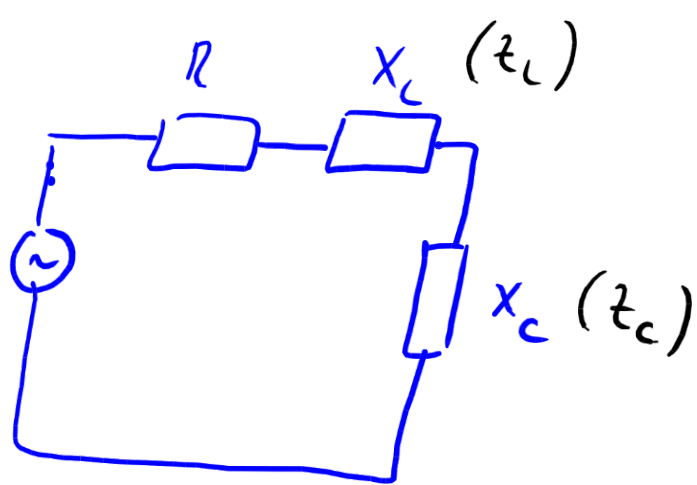
VEŠKOU NA VÝPOČTY S KOMPLEXNÍMI
ČÍSLY

ΠΕΡΙΘΩΡΑ ΑΣΙΩΝΟΔΟΣΩΝ

→ RLC V ΣΕΡΙΑ



Σημεία: R, L, C, U_0, ω
 $u = U_0 \sin(\omega t)$

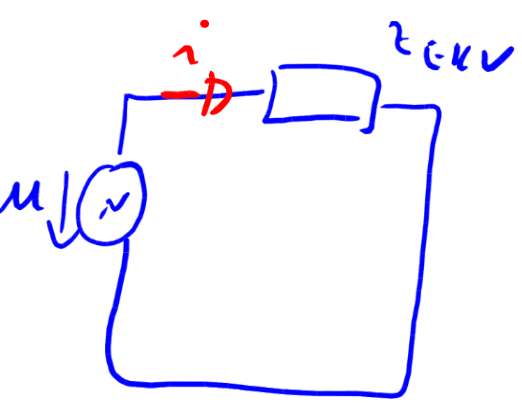


Σημεία μας:
 i, m_R, m_C, m_L
 (RESPECT. AMPLITUDE + PHASE POSITIVE)

REACTANCE 'X':
 (REACTIVE VALUE)
 $X_C = \frac{1}{\omega C}$... ΚΑΠΑΚΙΤΙΒΗ REACTANCE
 $X_L = \omega L$... ΙΝΔΟΥΚΤΙΒΗ

IMPEDANCE 'Z':
 (RESISTIVE VALUE)
 $Z_C = \frac{1}{j\omega C} \cdot \left(\frac{j}{j}\right) = \frac{-j}{\omega C} = -j \cdot X_C$
 $Z_L = j\omega L = j \cdot X_L$

ΕΚΙΒΑΛΕΝΤΙΑ ΟΙΚΟΥ



$$Z_{EKV} = R + Z_L + Z_C$$

$$Z_{EKV} = R + j\omega L - \frac{j}{\omega C}$$

$$Z_{EKV} = \underbrace{R}_{\text{RESISTANCE}} + j \underbrace{\left(\omega L - \frac{1}{\omega C}\right)}_{\text{REACTANCE}}$$

- ΥΠΟΛΟΓΙΣΤΕ ΠΡΟΩΔΗ

$$I_0 = \frac{U_0}{Z_{EKV}}$$

$$I_0 = A + jB$$

AMPLITUDE

$$|I_0| = \sqrt{A^2 + B^2}$$

PHASE POSITIVE

$$\varphi = \arctg\left(\frac{B}{A}\right)$$

+ ΠΟΤΩΡ ΝΑ II. Α III. ΚΥΑΔΙΣΜΟΙ

$$(A < 0)$$

Výpočet napětí:

$$U_R = I_0 \cdot R$$

$$U_C = I_0 \cdot Z_C$$

$$U_L = I_0 \cdot Z_L$$

AMPLITUDE + FÁZE ...

REZONANCE V RLC OBVODU

$$Z_{\text{ekv}} = R + j\underline{X} \quad X = 0$$

- V NAŠEM OBVODU:

$$X = \omega L - \frac{1}{\omega C} = 0 \quad / \cdot \omega C$$

$$\omega_{\text{rez}} = \sqrt{\frac{1}{LC}} \quad \dots \quad (\text{THOMPSONŮV VĚTAN})$$

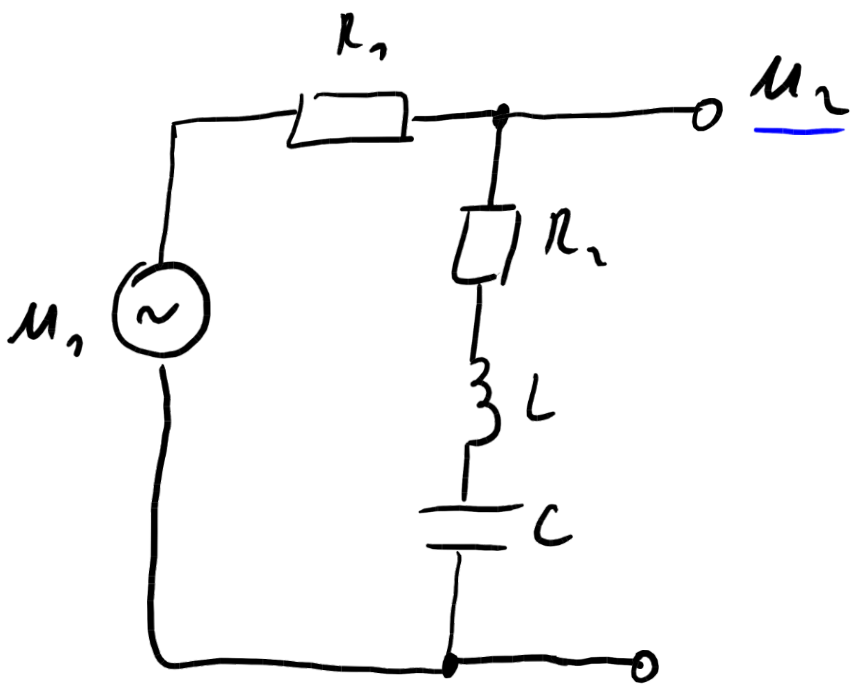
$$2\pi f_{\text{rez}} = \sqrt{\frac{1}{LC}}$$

$$f_{\text{rez}} = \frac{1}{2\pi\sqrt{LC}}$$

$$U_0 = U_R$$

$$U_C = -U_L$$
$$|U_C| = |U_L|$$

Dů: ZAPŘEMĚŘET VAD OBVODU

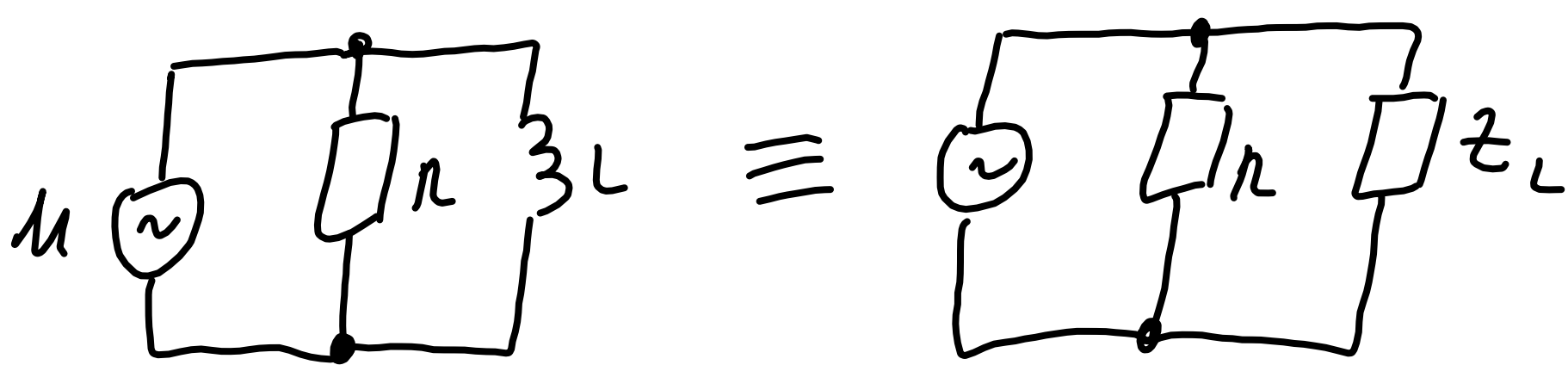


U_2 V REZONANCI

POČ. ODPOVĚDÍ PĚLICE

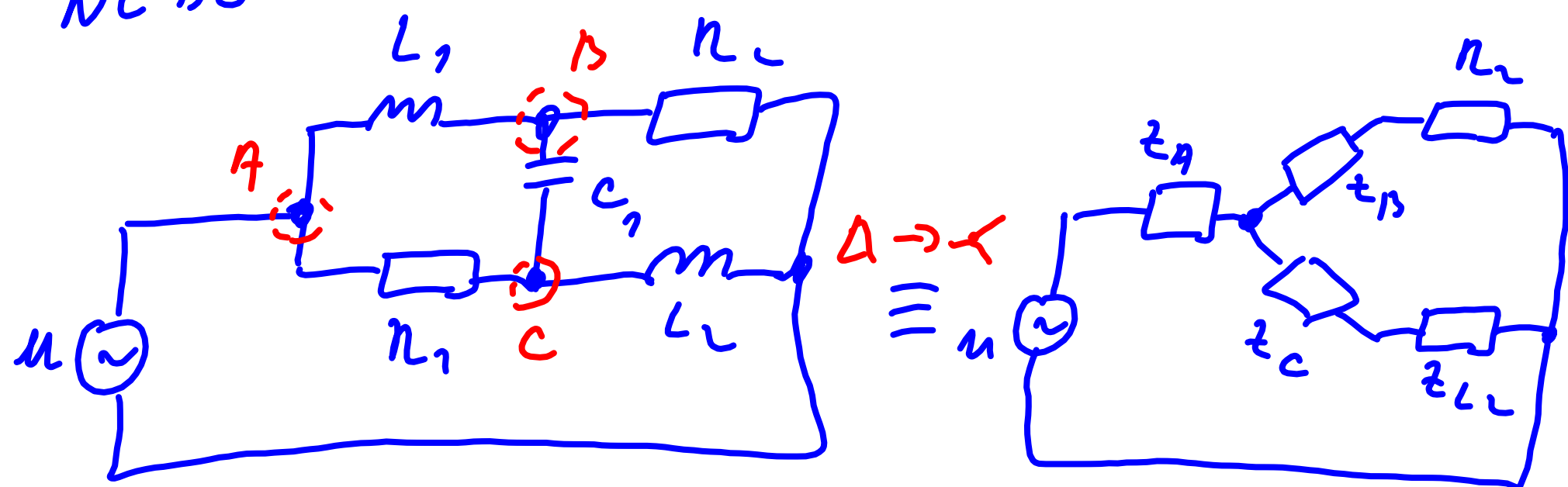
- NEBOJTE SE O STATNÍCH ZAPOJENÍ

NAPŘ. PARALELNÍ



$$z_{EKV} = \frac{R \cdot z_L}{R + z_L} = \frac{R \cdot j\omega L}{R + j\omega L}$$

NEBO

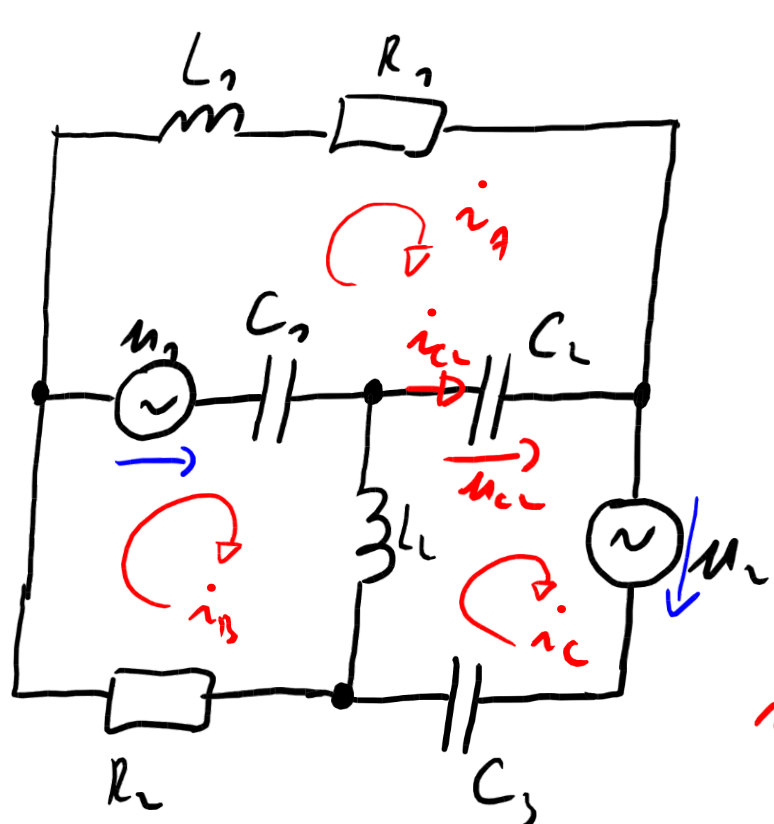


$$z_A = \frac{z_{L_1} \cdot R_1}{z_{L_1} + R_1 + z_{C_1}}$$

⋮

- SLOŽITĚJŠÍ OBVODY S VÍCE NAHŮJÍCÍMI ZDROJI

NAPŘ. SMYČKOVÉ Proudy



$$i_A: (z_{L1} + R_1) \cdot I_A + z_{C1}(I_A - I_C) + z_{C2}(I_A - I_B) - u_1 = 0$$

$$i_B: R_2 \cdot I_B + z_{C1}(I_B - I_A) + z_{L2}(I_B - I_C) + u_2 = 0$$

$$i_C: z_{C3} \cdot I_C + z_{L2}(I_C - I_B) + z_{C2} \cdot (I_C - I_A) + u_2 = 0$$

$i_{C1}, u_{C2} = ?$

SLAN (S KOMPLEXNÍMI ČÍSLY)

$$\begin{pmatrix} z_{L1} + R_1 + z_{C1} + z_{C2} & -z_{C1} & -z_{C2} \\ -z_{C1} & z_{C1} + z_{L2} + R_2 & -z_{L2} \\ -z_{C2} & -z_{L2} & z_{C3} + z_{L2} + z_{C2} \end{pmatrix} = A$$

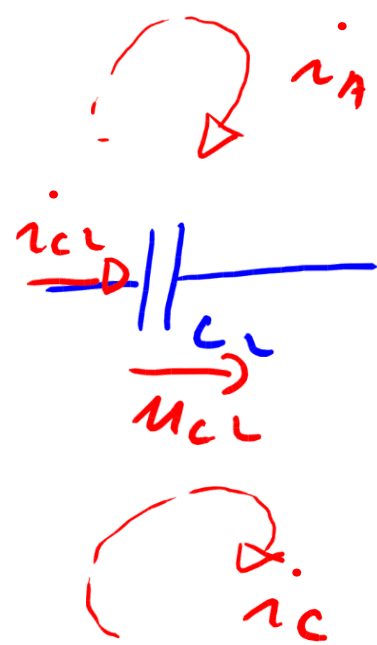
POZEV. MATICE JE SYMETRICKÁ

$$A \cdot \begin{pmatrix} I_A \\ I_B \\ I_C \end{pmatrix} = \begin{pmatrix} U_1 \\ -U_1 \\ -U_2 \end{pmatrix}$$

→ ŘEŠENÍ: MATURAS, CRANĚNOVO PRAVIDLO, ...

NAPŘ. $i_{c2} = ?$ $u_{c2} = ?$

$$i_{c2} = |I_{c2}| \cdot \sin(\omega t + \underline{\varphi_{c2}})$$



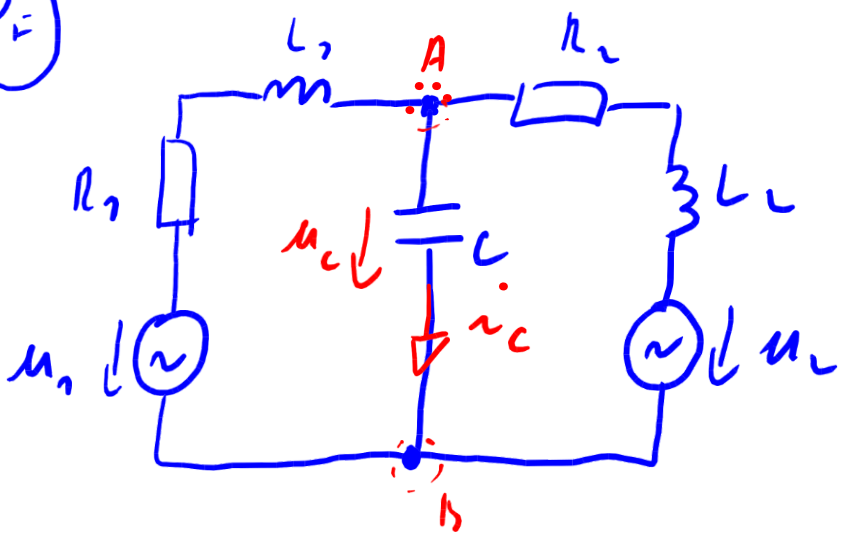
$$I_{c2} = I_C - I_A$$

$$u_{c2} = I_{c2} \cdot z_{c2}$$

komplexní
číslo
↓
AMPLITUDA $|I_{c2}|$
+ FÁZOVÝ POSUV φ_{c2}

THEVENINŮV TEORIE

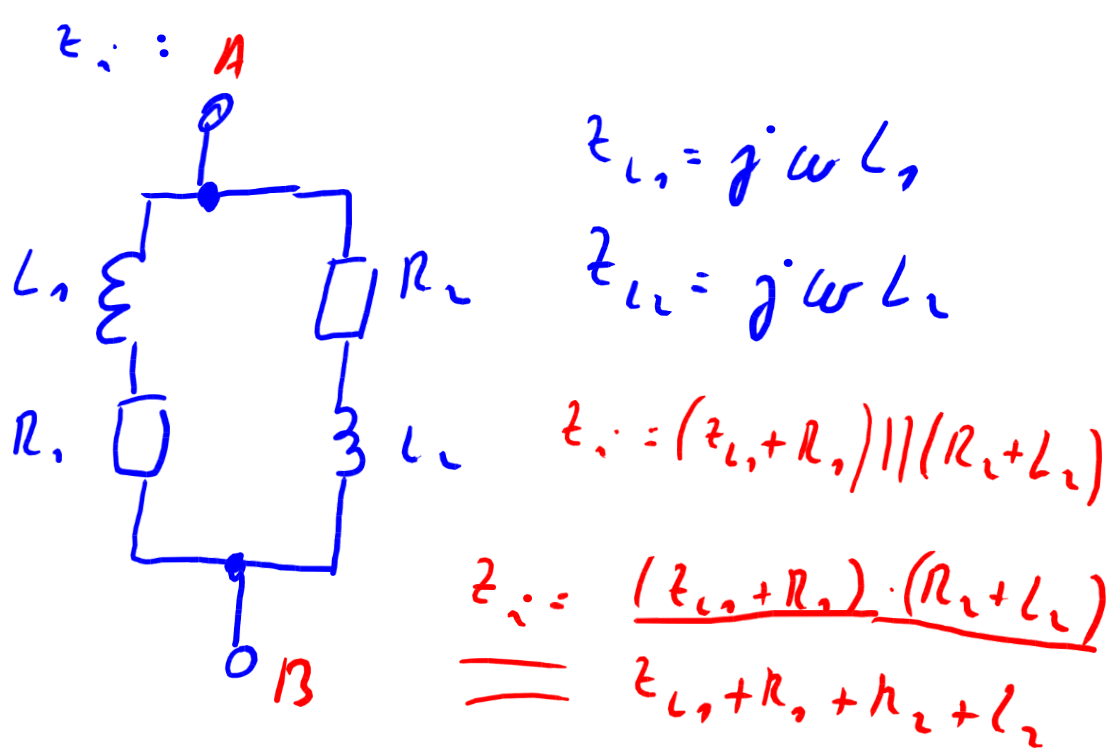
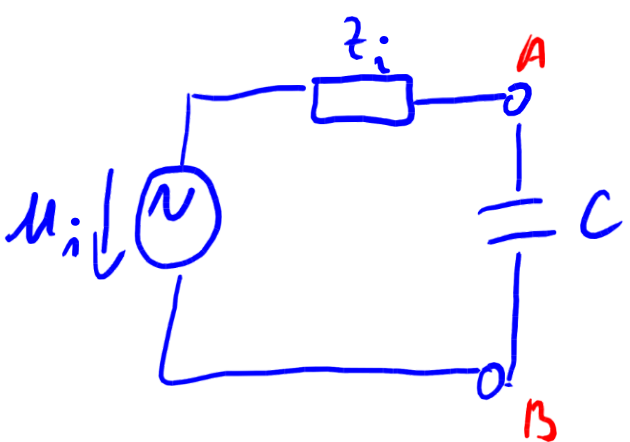
(P_i)



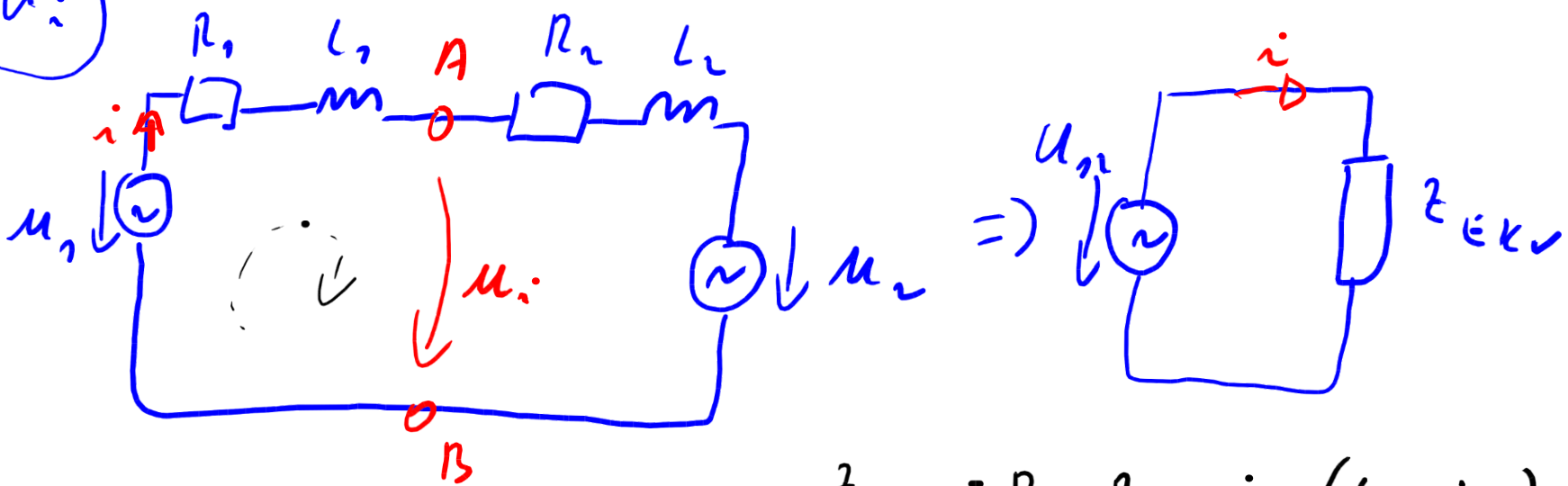
z nabíje: $R_1, R_2, L_1, L_2, C,$
 ω, u_1, u_2
 $u_1 = U_1 \sin(\omega t)$
 $u_2 = U_2 \sin(\omega t)$

 $i_c, u_c = ?$

EKVIVALENTNÍ OBVOD:



(U_i)



II. KIR. Z.

$U_{R1} + U_{L1} + U_i - U_1 = 0$

$U_i = U_1 - U_{R1} - U_{L1}$

$U_i = U_1 - I \cdot R_1 - I \cdot z_{L1}$ ✓

$z_{ekv} = R_1 + R_2 + j\omega(L_1 + L_2)$

$U_{n1} = U_1 - U_2$

$I = \frac{U_{n1}}{z_{ekv}}$

POZEV. II. K. Z.
 $I \cdot z_{ekv} + U_i - U_1 = 0$
 $I = \frac{U_1 - U_2}{z_{ekv}}$

$I_c = \frac{u_i}{z_i + z_c}, \quad U_c = I_c \cdot z_c$

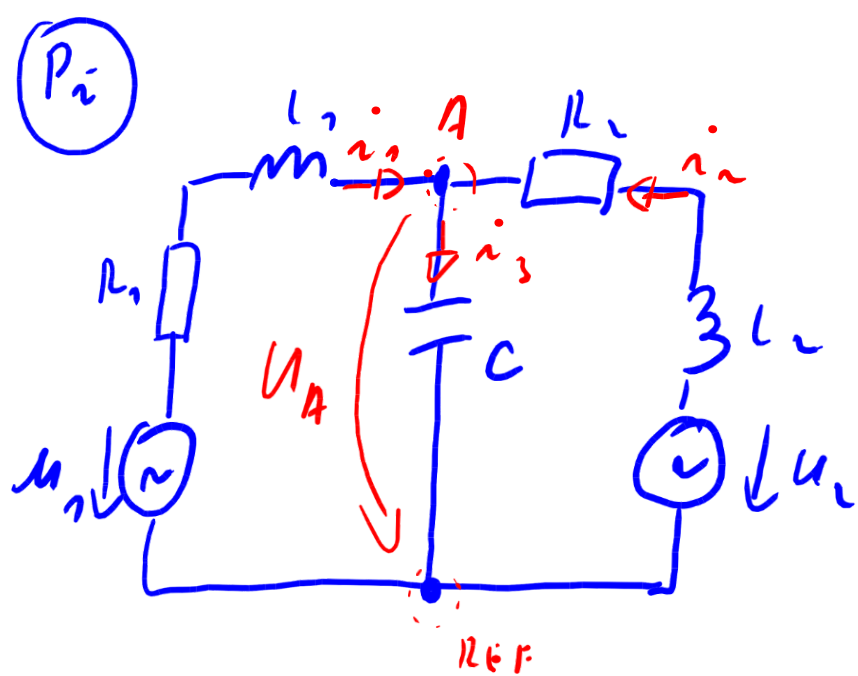
KOMPLEXNÍ ČÍSLA

AMPLITUDNÍ + FÁZ. POSUV

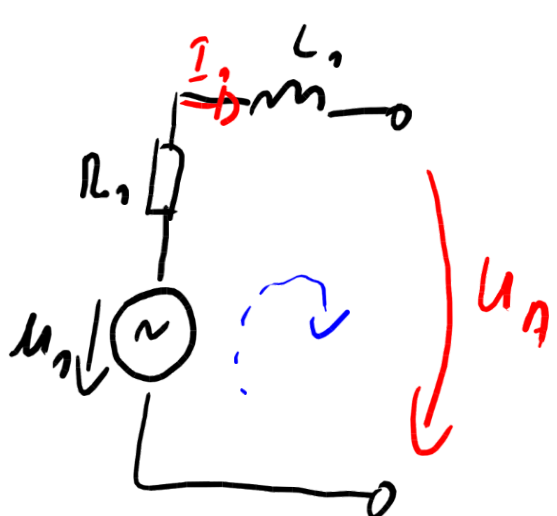
ΜΕΘΟΔΟΝ ΤΩΝ ΟΜΟΙΩΝ ΤΑΣΕΩΝ

ΥΠΕΡ ΤΗΝ Α (Ι.ΚΙΡ. ΤΗΝ ΚΟΝ)

$$i_1 + i_2 = i_3$$

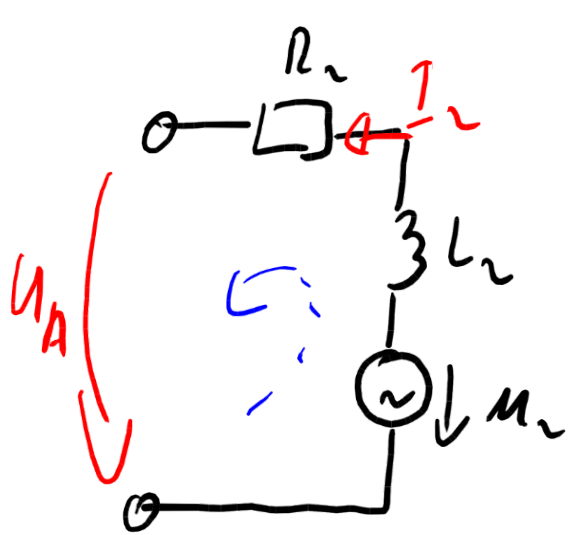


ΜΑΚΡΟΧΩΜΑΤΑ ΟΜΟΙΩΝ ΤΑΣΕΩΝ:



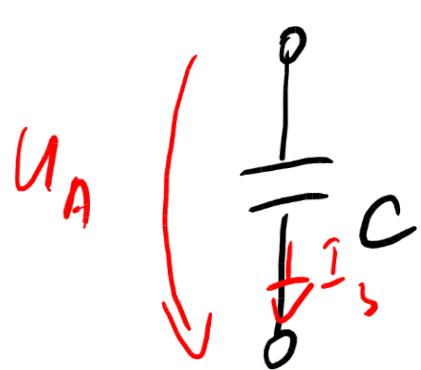
$$I_1 \cdot (z_{L1} + R_1) + U_A - u_1 = 0$$

$$I_1 = \frac{u_1 - U_A}{z_{L1} + R_1}$$



$$I_2 \cdot (z_{L2} + R_2) + U_A - u_2 = 0$$

$$I_2 = \frac{u_2 - U_A}{z_{L2} + R_2}$$



$$I_3 = \frac{U_A}{z_C}$$

$$\frac{u_1 - U_A}{z_{L1} + R_1} + \frac{u_2 - U_A}{z_{L2} + R_2} = \frac{U_A}{z_C}$$

⋮

$$U_A = \dots$$



$$U_C = U_A$$



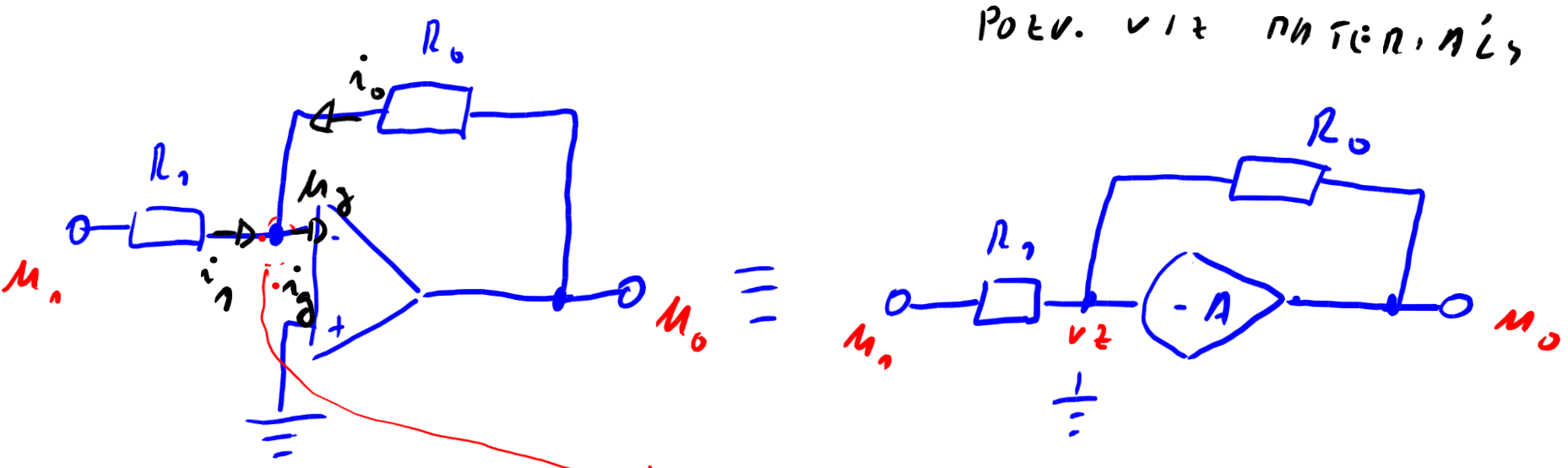
$$I_C = \frac{U_C}{z_C} = I_3$$



ΡΟΛΗΝ. ΠΑΤΛΑΒ

INVERTUJÍCÍ OPERAČNÍ ZESÍLOVAČ (IDEÁLNÍ)

POEV. VIZ PRŮBĚH, AŽ K P>K



→ I. KIR. ZÁKON
 $i_o + i_1 = i_g$

VLASTNOSTI:

- $A = \infty$
- $R_{in} = \infty$
- ($R_{out} = 0$)

$$i_g = 0A \left(\frac{u_g}{R_{in}} \right)$$

$$u_o = -A \cdot u_g$$

$$u_g = \frac{u_o}{-A} = \frac{u_o}{-\infty} = \underline{\underline{0V}} \dots VZ$$

$$i_1 = \frac{u_1 - u_g}{R_1} = \frac{u_1}{R_1}$$

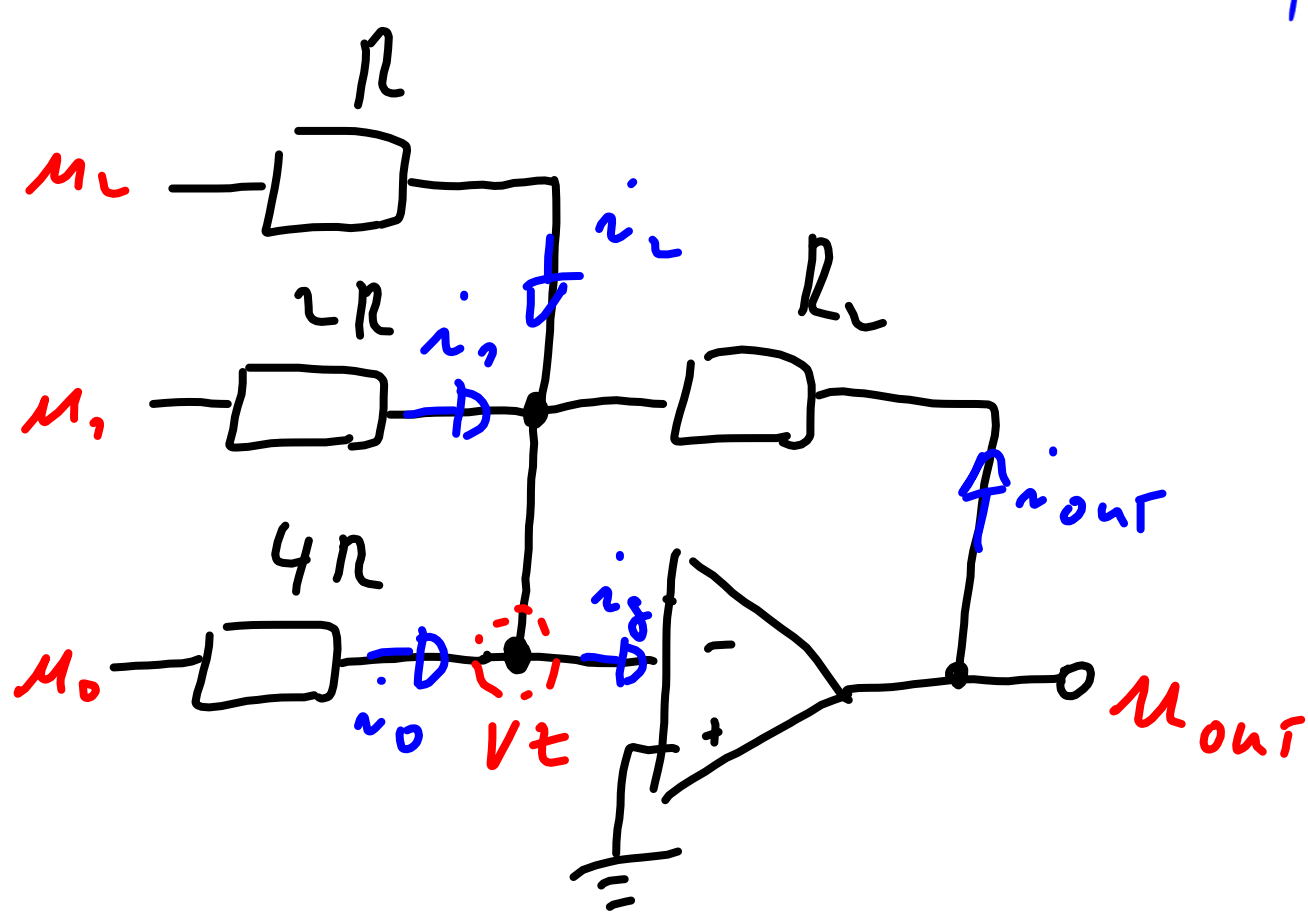
$$i_o = \frac{u_o - u_g}{R_o} = \frac{u_o}{R_o}$$

$$\frac{u_1}{R_1} + \frac{u_o}{R_o} = 0 \rightarrow \boxed{u_o = - \underbrace{\frac{R_o}{R_1}}_A \cdot u_1}$$

$R_o = R_1 \dots$ INVERTOR

SCÍTAČKA (INVERTUJÍCÍ)

POK. D/A PŘEVODNÍKY



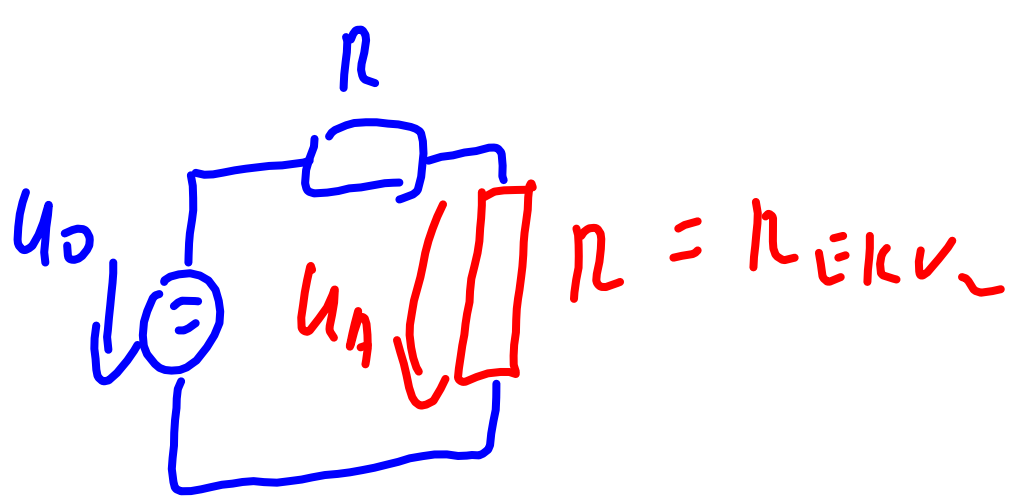
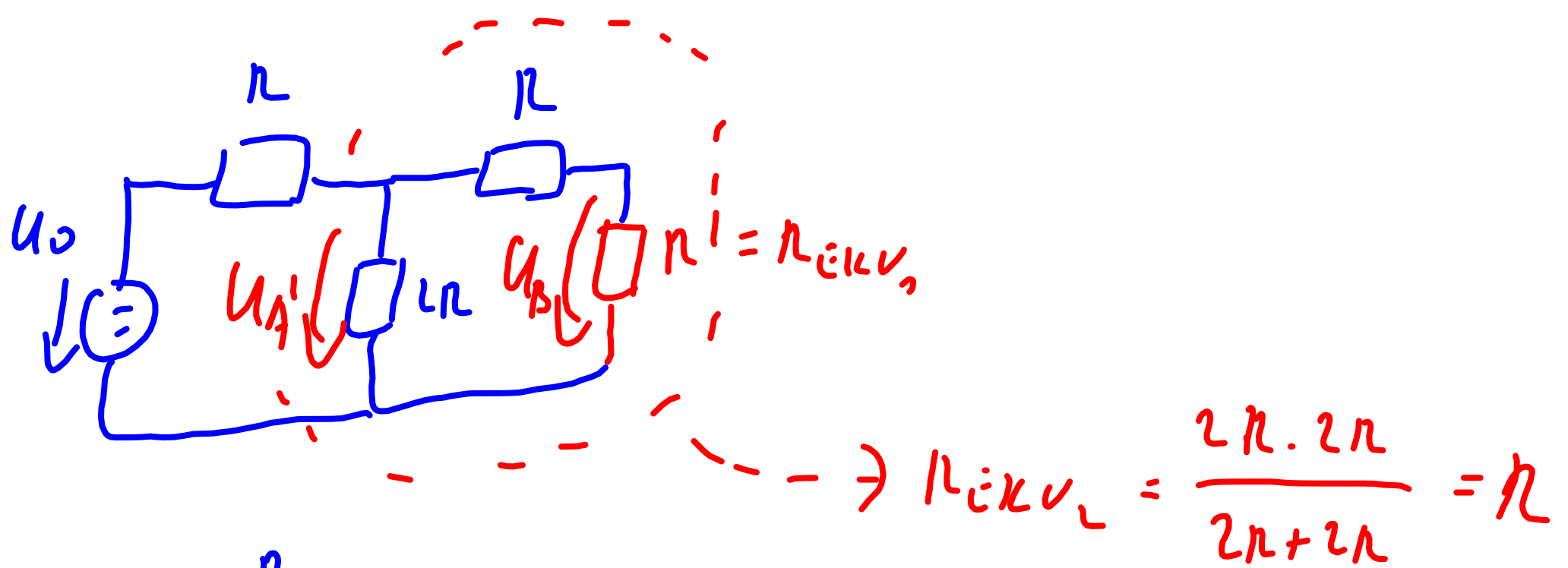
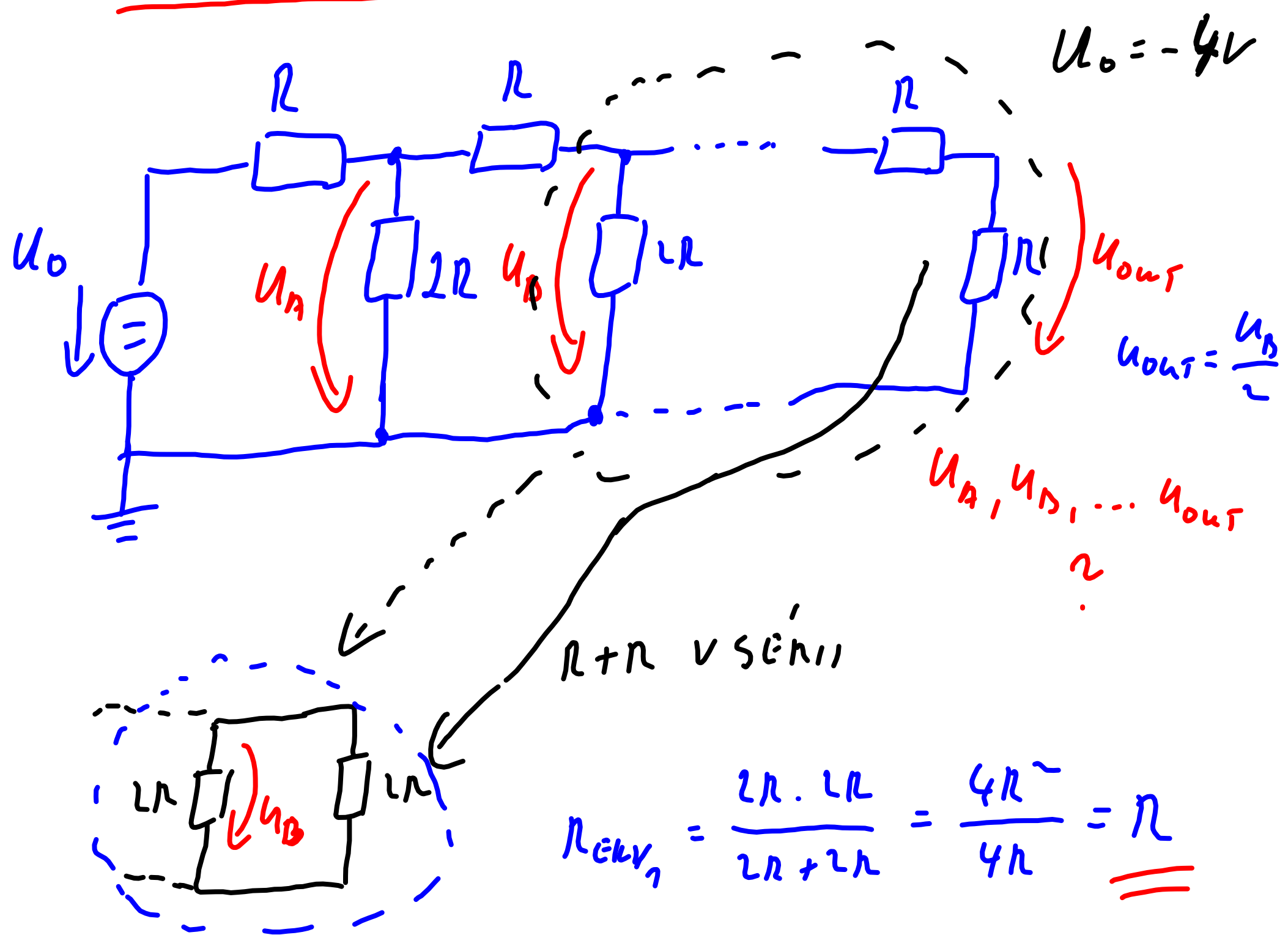
I. KIR. ZÁKON:

$$i_0 + i_1 + i_2 + i_{out} - i_g = 0$$

$$\frac{u_0}{4R} + \frac{u_1}{2R} + \frac{u_2}{R} + \frac{u_{out}}{R} = 0$$

$$u_{out} = -\frac{R_f}{R} \left(\frac{u_0}{4} + \frac{u_1}{2} + \frac{u_2}{1} \right)$$

R - 2R ELEKTRICKÝ OBVOD



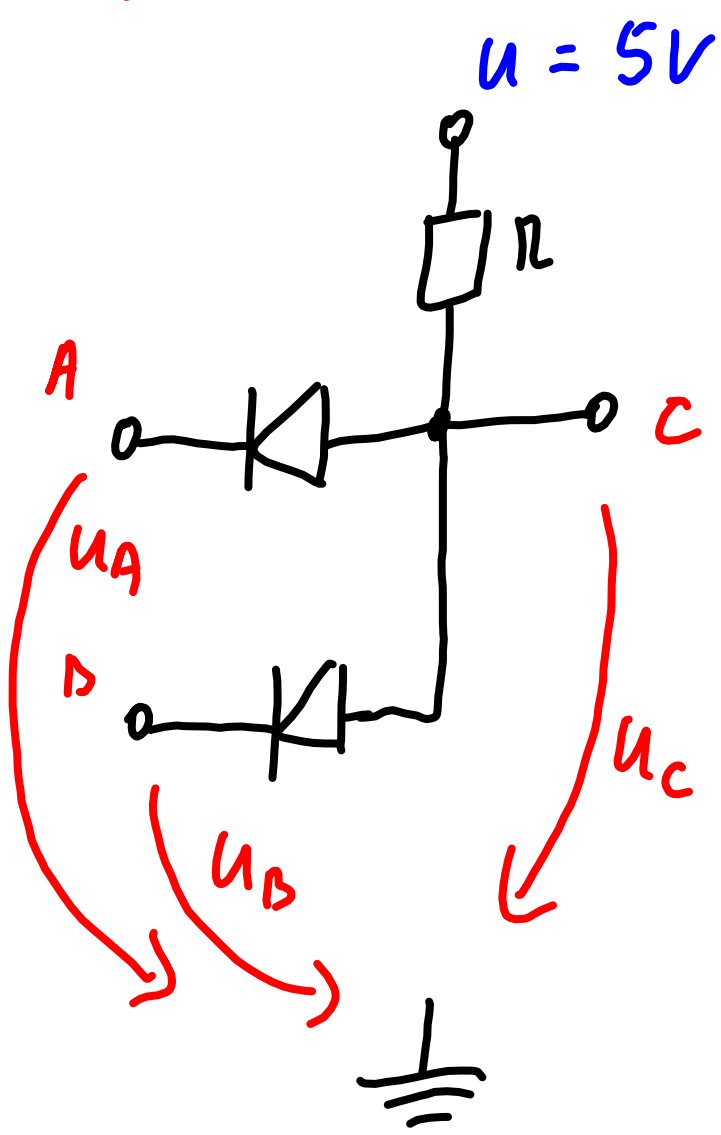
$$U_A = \frac{1}{2} U_0$$

$$U_B = \frac{1}{2} U_A$$

$$\vdots$$

$$U_{out} = \frac{1}{2} U_F$$

ANALYZOVAT LOGICKÝ OBRVOD S DIODAMI

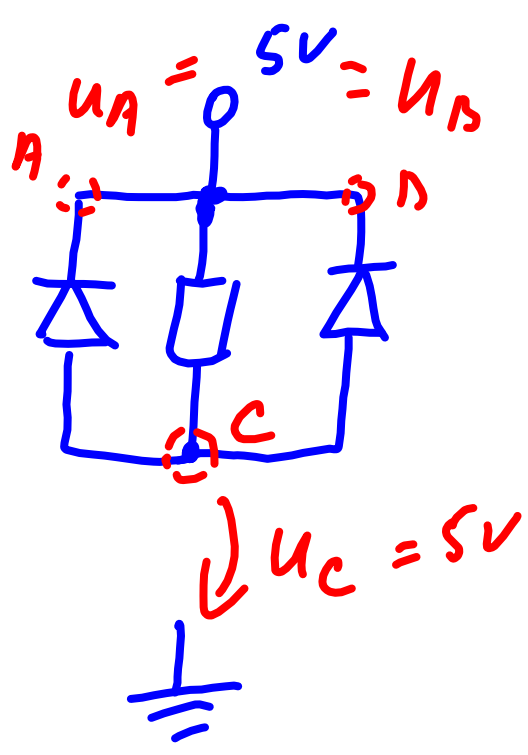
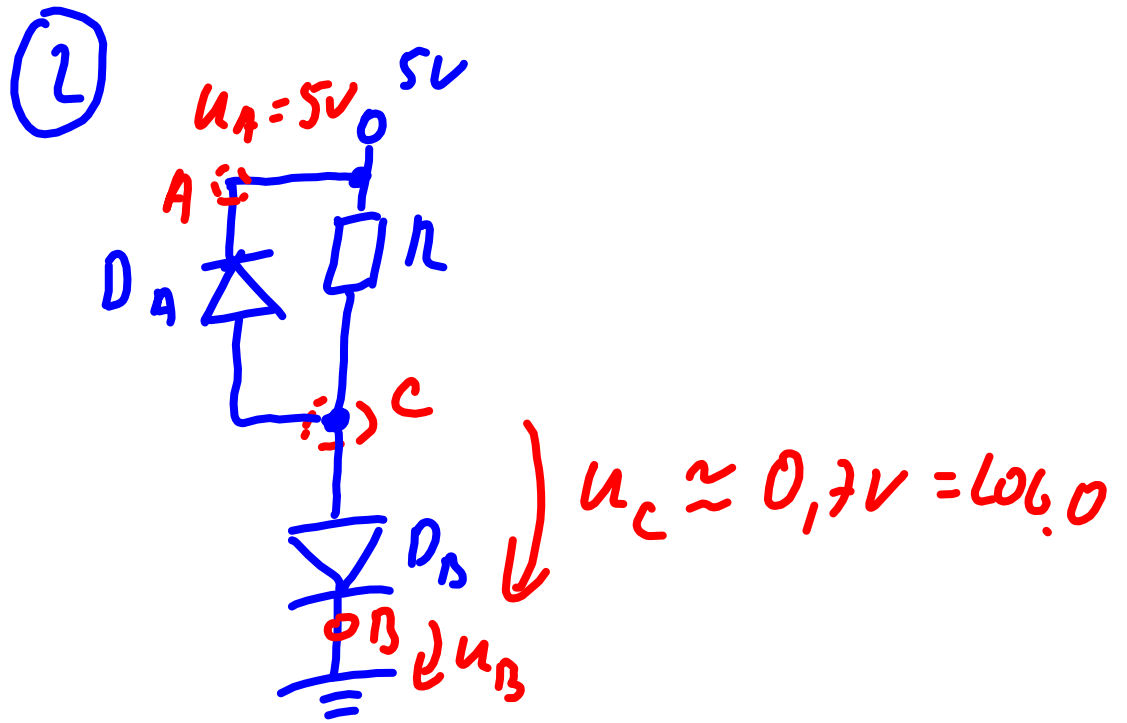
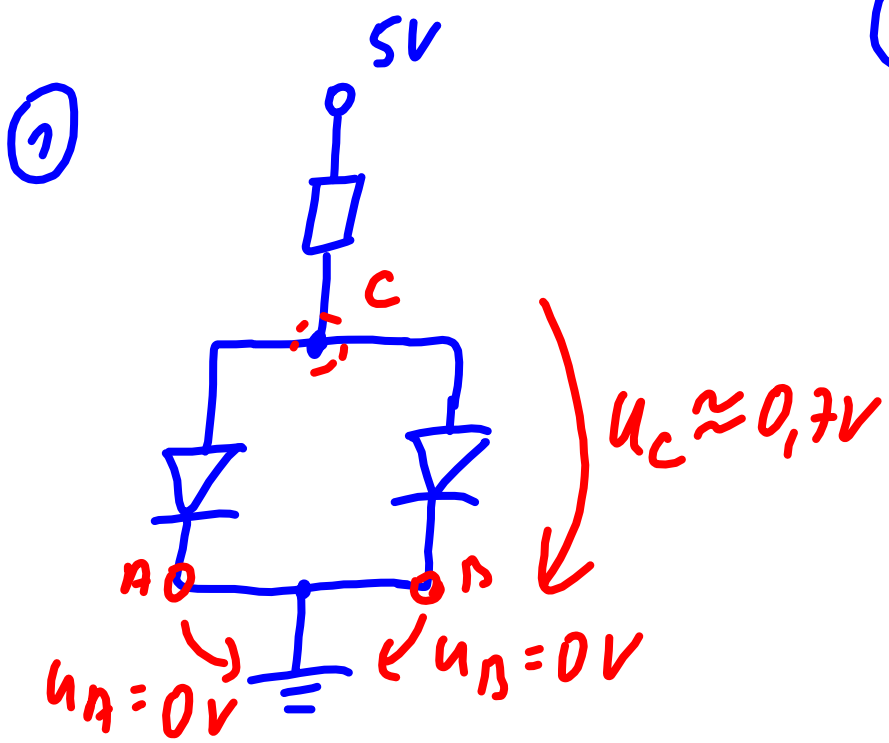


LOG. 0 = 0-2V
LOG. 1 = 3V-5V

LOGICKÉ HODNOTY

	VSTUP		VÝSTUP
	A	B	C
①	0	0	0
	0	1	0
②	1	0	0
③	1	1	1

AND



OR

